# TACTICAL HF FIELD EXPEDIENT ANTENNA 

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Gurkan Turkes
March 1990

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## TACTICAL HF FIELD EXPEDIEST ANTEN:NA PERFORMANCE VOLUME I

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The results of this study can be included in an antenna engineering handbook and can be used to interface with existing ionospheric propagation codes in order to obtain optimum communication effectiveness.

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#### Abstract

This thesis investigates the performance of various configurations of tactical High Frequency (HF) field deployable antennas in the presence of lossy earth. Antennas investigated include horizontal dipoles, short sloping wires, inverted vees, and monopoles with buried and elevated radials. Numerical models of the antennas are exercised via the Numerical Electromagnetics Code (NEC) for radiation pattern performance. Antennas are analyzed for applicability to (1) short-range Near Vertical Incident Skywave (NVIS), where high elevation radiation angles are required. ;2) medium- and longarange low radiation angle use, and (3) vertically polarized low-angle radiation for ground wave communication. Good .VVIS and ground wave performance occurs for horizontal dipoles. Sloping wires and sloping dipoles are similar to horizontal dipoles but exhibit a moderate amount of azimuth plane direntivity. Vertical monopoles witt at least 15 buried radials produce medium- and long-range skywave coverage and good ground wave performance. Four elevated radials for quarter-wavelength monopoles are shown to out-perform 15 buried radials and are much easier to erect. The larger and more difficult-to-erect inverted vee dipole slightly outperforms a monopole by virtue of modest azimuth plane directivity:

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## I. INTRODUCTION

## A. BACKGROUND

The military forces of today have the capability to be highly mobilc, strike quickly over long distances, and integrate complex intelligence resources and weapon systems to effectively deliver combat power at critical points. The control and coordination of these capabilities reiy on dependable communications. To support the complex nature of the modern battlefield, the military employs numerous and varied communication systems.

Before the advent of satellites, long range communications were routed over high frequency ( HF ) skywave paths. HF technology has been relatively neglected as satellite communications are more reliable and the data rate is much higher than HF links. But in a worst-case operational scenario, the assumption would have to be made that satellite communications would be impossible. In this situation all essential external communications would have to be made with HF communication systems. HF communication systems provide the military short-, medium-, and long-range communication for voice, digitally coded burst messages, radio teletype traffic, and radio telegraph. Users of military HF communications vary from special operation teams which are operating in isolated areas to major military command headquarters which control joint service operations.

The high frequency ( HF ) band covers frequencies between the 3 and 30 MHz as defined by the International Radio Consultative Committec (CCIR). For the HF band, there are two possible propagation modes, skywave and ground wave, where the skywave is the dominant mode of propagation.

The changing conditions of the ionosphere efiect the useful extent of the HF band. For example, the ionosphere varies in density over :

1. 24 hour cy.cle
2. 4 season cycle
3. 11 year cycle
as well as randomly due to solar disturbances.
In this thesis, the following set of HF tactical antenna model configurations were analyzed at 3.8.7.2, 14.2, 21.3, and 28.5 MHz frequencies that cover the HF band:

- Half-wavelength horizontal dipole
- Half-wavelength inverted vee dipole
- Half-wavelength sloping dipole
- Quarter-wavelength sloping wire
- Quarter-wavelength monopole with 4 ft ground rod
- Quarter-wavelength monopole with 4,15 , and 30 radial wircs, one quarterwavelength long, buried 2 inches deep or elevated 0.08 wavelengths high.

The results of this study can be used to interface with existing ionospheric propagation codes in order to obtain optimum communication effectiveness.

## B. IMPORTANT ANTENNA PARAMETERS

Antenna parameters such as input impedance, average power gain, length, height above ground, number of radials and the position of them with respect to the ground, ground rods, sloping angles for dipoles, and the feed points were varied. The effect of the input impedance on the radiation pattern is one of the most important observable and controllable factors. The input impedance of an antenna is the impedance presented by the antenna at its terminals and is composed of real and imaginary parts [Ref. 1],

$$
\begin{equation*}
Z_{l n}=R_{l n}+j X_{l n}^{\prime} \tag{1}
\end{equation*}
$$

where $Z_{r r}$ is the antenna impedance, $R_{i n}$ is the antenna resistance, and $X_{i n}$ is the antenna reactance. The resistive part consists of two components,

$$
\begin{equation*}
R_{l n}=R_{L}+R_{r}, \tag{2}
\end{equation*}
$$

where $R_{L}$ is the loss resistance and $R_{r}$ is the radiation resistance of the antenna:
The loss resistance $R_{L}$ represents both power dissipated on the antenna structure and associated hardware as heating losses and power dissipated in the ground because of the ground-system losses. The radiation resistance $R$, is a form of dissipation and represents power that leaves the antenna as radiation and never returns. On many antennas, the loss resistance is small compared to the radiation loss [Ref. 1].

The antenna impedance is important for transfer of power from a rransmitter to an antenna or from an antenna to a receiver. For example, to maximize the power transferred from a receiving antenna, the antenna impedance should be a conjugate match which means a load of equal resistances and equal magnitude and opposite sign reactances. Finally; it should be noted that the antenna impedance for receiving and transmitting is the same as a consequence of reciprocity [Ref. 1].

## C. BASIC THEORY OF THE ANTENNAS

## 1. Half-Wavelength Dipole

This is a very widely used antenna. It has a linear current distribution whose amplitude varies as one-half of a sine wave with a maximum at the center [Ref. 1].

The advantage of a half-wavelength dipole is tiat it can be made to resonate and present a zero input reactance. The real part of the input impedance (the input resistance) represents far field losses (i.e., dissipation). The current distribution of the half-wavelength dipole is

$$
\begin{equation*}
I(z)=I_{m} \sin \left[\beta\left(\frac{\lambda}{4}-|z|\right)\right], \tag{3}
\end{equation*}
$$

where $|z| \leq \frac{\lambda}{4}$ and $\beta=\frac{2 \pi}{\dot{\lambda}}$.
This current goes to zero at the ends $\left(z= \pm \frac{\dot{j}}{4}\right)$ and its maximum value $I_{m}$ occurs at the center $(z=0)$ as seen in Fig. la [Ref. 1].

Starting from this current formula the complete (i.e., normalized) far-field pattern can be obtained as [Ref. 1]

$$
\begin{equation*}
F(\theta)=g(\theta) /(\theta)=\frac{\cos \left[\left(\frac{\pi}{2}\right) \cos \theta\right]}{\sin \theta}, \tag{4}
\end{equation*}
$$

Where $g(\theta)$ is called the element factor and $f(\theta)$ is called the normalized pattern factor. The $\theta$ variation of the function $F(\theta)$ determines the far-field pattern as seen in Fig. 1b [Ref. I].
2. Vee Dipole
"This antenna can be visualized as an open circuit transmission line that has been bent so that ends of length (h) have an included angle $y$ as seen in Fig. 2 [Ref. 1]."

The input impedance of a vee dipole is generally less than a straight dipole of the same length. The directivity of a vee dipole can be greater than that of a straight dipole. The corresponding directivity of the vee dipole is [Ref. 1]

$$
\begin{gather*}
D=2.94\left(\frac{h}{\lambda}\right)+1.15  \tag{5}\\
D_{d B}=10 \log (D) \tag{6}
\end{gather*}
$$

Figure 3 is a typical radiation pattern (elevation) of the inverted vee dipole.


Figure 1. The half-wavelength dipole: (a) Current distribution I(z) (b) Radiation pattern $F(\theta)$ (From Ref. 1)

## 3. Monopole

"A monopole is a dipole divided in half at its center feed point and fed against a ground plane. High frequency monopoles are often fed from coaxial cables behind the ground plane as seen in Fig. 4." [Ref. 1]

The currents and charges on a monopole are the same as on the upper half of its dipole counterpart. The principles of image theory are applicable and the terminal voltage is half that of the dipole because the gap width of the input terminals is half that of the dipole and the same electric field over half the distance gives half the voltage. The input impedance for a monopole is therefore half of its dipole counterpart as is the radiation resistance and input power.

$$
\begin{equation*}
Z_{I N, M O N O}=\frac{1}{2} Z_{I N, D I P O L E} \tag{7}
\end{equation*}
$$



Figure 2. The vee dipole antenna: (From Ref. 1)

$$
\begin{equation*}
R_{r, M O N O}=\frac{1}{2} R_{r, D I P O L E} \tag{8}
\end{equation*}
$$

The radiation pattern of a monopole above a perfect ground plane is the same as that of a dipole similarly positioned in free space, since the fields above the image plane are the same.

## D. INFORMATION ABOUT GROUND

The operation of HF antennas which usually are wire antennas is affected significantly by the presence of typical environmental surroundings such as the earth, buildings, etc. A ground plane can take many forms, such as radial wires around a monopole, the roof of a car, or the real earth (i.e., ground). In many situations the earth is well approximated as being infinite and planar, but it is a poor conductor. In the Antenna Engineering Handbook, practical ground types are considered under six different categories as seen in Table 1 [Ref. 2].

In this thesis, the various configurations of the antennas were investigated over fair (average) ground. The reason fair ground was chosen is because there are many configurations of the antennas and five different frequencies. Fair ground also has average values of permittivity and conductivity, compared to other ground types.

## INV. VEE DIP. $H=7.62 \mathrm{M}=25^{\prime} \mathrm{FR}=14.2 \mathrm{MHZ}$ L $二 \mathrm{LAMBDA} / 2$

ELEVATION PAT. EPS $=10, \mathrm{SIG}=.003$


Figure 3. The elevation pattern of the half-wavelength inverted vee dipole


Figure 4. The monopole antenna fed from a coaxial cable: (From Ref. 1)

The effect of imperfect ground, which has low conductivity compared to perfect ground, is more ohmic losses. The electric fields penetrate into the earth and excite currents. These currents give rise to ohmic losses which appear as an increase in the input ohmic resistance. Therefore the radiation efficiency of the antenna decreases [Ref. 1] as

$$
\begin{equation*}
e=\frac{\dot{R}_{r l}}{R_{r l}+R_{O H M I C}}=\frac{R_{r l}}{R_{I N}}, \tag{10}
\end{equation*}
$$

where e is the radiation efficiency, $R_{n}$ is the radiation resistance, $R_{\text {oнмIC }}$ is ohmic resistance, and $R_{I N}$ is the input resistance.

The pattern of an antenna over finite ground is different from the pattern when the antenna is operated over a perfect ground plane. By using image theory, approximate patterns can be obtained. The Numerical Electromagnetics Code ( $\mathcal{N E C}$ ) includes the Fresnel plane wave reflection coefficient method for modeling structures over ground. This method is fast but of limited accuracy and should not be used for structures very close to the ground.

Table 1. GROUND TYPES (FROM REF. 2).

| Conductivity <br> $($ mhos m$)$ | Relative <br> permittivity | Land type |
| :---: | :---: | :---: |
| 0.00022 | 2.5 | flat desert, cities |
| 0.0012 | 7.0 | mountains;steep rocky hills |
| 0.003 | 10.0 | average ground |
| 0.011 | 13.0 | pastoral land, medium hills |
| 0.065 | 22.5 | rich farm land |
| 0.15 | 34.0 | rice paddy |

There is another method which is called Sommerfeld Norton for wire antennas only. This method was used in this research since it is more accurate for structures which are close to ground although it is slower and requires more memory space. The Sommerfeld, Norton method requires a separate computer program (SOMNTX) to be run prior to $\lambda E C$ in order to generate and store a " Ground Interaction Matrix " which is then called by XEC .

The losses in an earth ground can be reduced by providing a highly conductive return path. This is usually achieved with a Radial Wire Ground System which produces a pattern more nearly like that for a perfect ground, increasing low elevation angle radiation which is very useful for long distance communications. The radial wires can be laid on top of the ground or buried slightly beneath it. In fact, they need not be buried, but it is usually convenient to do so; however, they should not be buried too decp. For high-power transmitting antennas it is important to have a well designed radial system to achieve high efficiency.

## II. NUMERICAL METHODS AND TECHNIQUES FOR ANTENNA ANALYSIS

## A. ANTENNA MODELING AT THE NAVAL POSTGRADUATE SCHOOL

At present, there are two widely used antenna modeling programs which are available at NPS. They are the Mini-Numerical Electromagnetics Code (MININEC) which runs on a personnel computer (PC) and the Numerical Electromagnetics Code (NEC) which runs on a mainframe computer and on a PC.

## B. THE NUMERICAL ELECTROMAGNETIC ENGINEERING DESIGN SYSTEM (NEEDS)

As a system, , $\operatorname{CEEDS}$ consists of a package of programs and operates on a PC,XT or PC:AT computer. The programs are MININEC and NEC2 for antenna modeling; IGLANA, a graphics utility system; GRAPS for ploting; and several auxiliary programs.

1. MININEC

MININEC is an interactive program which is useful for many applications in wire antennas. especially for small problems.
a. Capabilities

Although it has limited capabilities. MININEC is a good tool for antenna analysis and design. The capabilities of MININEC are [Rer. 3]:

- Lp to 10 wires and 75 unknowns (segments) may be used in constructing a MININEC model.
- Antemnas can be modeled either in free space or over perfectly conducting ground.
- Electric and magnetic fields (near and far) can be calculated.
- Solutions can be obtained for impedances and currents on wires.
- Far fields can be calculated in either volts per meter or in terms of power radiation pattern.
- Lumped parameters (such as loading coils and traps) can be included in a MININEC model.
- Fresnel reflection coefficient correction of radiation patterns may be included in MININEC models via up to five changes in ground surface impedance. The ground model may resemble either a sircular or cliff model.
b. Limitations


## Limitations of MININEC are [Ref. 3]:

- The number of wires and segments can be used in modeling are limited. Only simple structures or a simplification of larger structures can be modeled.
- MINI.NEC can not perform surface modelings via a surface current patch.
- MININEC can not be used for antennas closely coupled to finite ground.

2. GRAPS

GRAPS is a program designed for plotting output data from MININEC, NEC, or general data. It is menu-driven and written in BASIC. The various types of GRAPS plots are linear, bilinear, log-linear, polar, Smith, and log-log [Ref. 4].
3. NEC 2
$\therefore E C 2$ is a version of $\wedge E C$ limited to structures which are in free space or above the earth [Ref. 5].
4. INTERACTIVE GRAPHICS UTILITY FOR AUTOMATED NEC AㅊALYSIS (IGLA..AA)

This system was developed to reduce the time required for $\times E C$ antenna model evaluation by providing partial automation to both the data entry and the data display processes. In particular, IGUA入A simplifies modeling of structures by allowing use of a digitizer or mouse to input views of a structure. This data can then be edited and combined with other views of the object to produce a three-dimensional model. Facilities are included for user input of required control and documentation cards, data transmission to a mainframe host computer, and display of $\searrow$ EC output data [Ref. 6].

## C. THE NUMERICAL ELECTROMAGNETICS CODE-(NEC-3/MAINFRAME)

## 1. INTRODCCTION

All antennas from this thesis have been modeled using the . Numerical Electromagnetics Code, Version 3 ( $\mathcal{E C}-3$ ) with double-precision accuracy on the IB.M 3033 computer, while $\lambda E E D S$ was used as an auxiliary tool. It is a user-oriented computer code written in FORTRA. 1 and the most capable and flexible tool available at $\uparrow$ PS for electromagnetic nodeling of wire antennas. Because it is a powerful and complex tool. a considerable learning process is required to master its capabilities. Technically, XEC is used to analyze antennas or other metal structures based on the use of numerical solutions of integral equations for currents induced on the structure by an incident plane wave or a voltage source. . EEC -3 has the following capabilities [Ref. 7] :

- Up to 300,1000 , or 2000 wire segments, depending on the version of $\triangle E C$ being used.
- Up to 150,500 , or 1000 surface patches.
- More rapid computations than obtained using NEC2 on a PC.
- Convenient storage of NEC datasets and results, and ready accessibility to data.
- A library of useful PROGRAMS, EXECS, and data handling utilities (see Appendix A)

The NEC codes use both an electric field integral equation (EFIE) and a magnetic field integral equation (MFIE) to solve general electromagnetic radiation problems. The solution is obtained by using the method of moments.
2. ELECTRIC FIELD INTEGRAL EQUATION (EFIE)

In solving for the current, two approximation options are available in NEC, the thin-wire kernel and the extended thin-wire kernel. For thin-wire the current on the surface of segment is reduced to a filament of current on the segment axis. Using the extended thin-wire kernel, a current is uniformly distributed around the segment surface. The EFIE used in $\mathcal{N E C}$ is given in [Ref. 7]:

$$
\begin{equation*}
-\hat{s} \cdot \bar{E}^{\prime}(\bar{r})=\frac{-j}{4 \pi \omega \varepsilon} \int_{c(\bar{f})} I\left(s^{\prime}\right)\left(\hat{s} \cdot \hat{s}^{\prime} k^{2}-\frac{\hat{o}^{2}}{\hat{o}_{s} \hat{\sigma}_{s^{\prime}}}\right) g\left(\bar{r}, \bar{r}^{\prime}\right) d s^{\prime} \tag{11}
\end{equation*}
$$

where:

| $\hat{s}$ | $=$ unit vector along the wire axis. |
| :--- | :--- |
| $s^{\prime}$ | $=$ distance along the wire axis. |
| $\overline{E^{\prime}}(\bar{r})$ | $=$ incident electric field at r. |
| $\omega$ | $=2 \pi f$, where f is the frequency. |
| $I\left(s^{\prime}\right)$ | $=$ axial current. |
| $\varepsilon$ | $=$ permittivity. |
| k | $=\omega \sqrt{\mu \varepsilon}=$ phase constant. |
| $\bar{r}$ | $=$ observation point. |
| $\bar{r}^{\prime}$ | $=$ source point |
| $g\left(\bar{r}, \bar{r}^{\prime}\right)$ | $=\operatorname{cxp}\left[\frac{-j k r}{R}\right]=$ free space Green's function. |
| R | $=\left(\bar{r}-\bar{r}^{\prime}\right)$ |

3. MAGMETIC FIELD INTEGRAL EQLATION (MFIE)

入EC includes a patch option for modeling surfaces using the MFIE. This formulation is restricted to closed surfaces with nonvanishing enclosed volume. The MFIE used in $\perp \mathrm{EC}$ is given in [Ref. 7]:

$$
\begin{equation*}
\bar{J}_{s}(\bar{r})=2 \hat{n} \times \bar{H}^{i n c}(\vec{r})+\frac{1}{2 \pi} \hat{n} \times \int_{s} \bar{J}_{s}\left(\bar{r}^{\prime}\right) \times \nabla^{\prime} g d s^{\prime} \bar{r} s^{\prime} \tag{12}
\end{equation*}
$$

where:

$$
\begin{array}{ll}
\bar{J}_{s}(\bar{r}) & =\text { surface current density. } \\
\left.\bar{H}^{\ln ( } \bar{r}\right) & =\text { incident magnetic field at the observation point. } \\
\hat{n} & =\text { unit vector normal to the surface. }
\end{array}
$$

## D. WIRE MODELING GUIDELINES

Short straight segments for wires and the flat patches for surfaces are the basic devices for modeling structures with NEC. Since only wire antennas were investigated in this thesis, guidelines are given for modeling wire antennas.

An antenna and any other conducting object in its vicinity that affect performance must be modeled with strings of segments following the paths of the wires. Proper choice of segments is the most critical step in obtaining accurate results. For accuracy and efficient run-time, the number of segments should be the minimum required.

A wire segment is defined by the coordinates of its two end points and by its radius. Geometrical and electrical guidelines for segments are given below [Ref. 7]:

1. Geometrically, segments should follow the paths of conductors as closely as possible.
2. Each wire must be broken into segments of length $\Delta$, where

$$
0.1 \lambda<\Delta<0.001\rangle
$$

and $\lambda$ is the wavelength of the desired frequency.
 antenna.
4. Lising extremely short segments, less than about $10 \mathrm{E}-3 \dot{1}$, should be avoided since it may lead to numerical inaccuracy.
5. The wire radius must be small compared to the segment length $\Delta$. For the thinwire kernel approximation, $\frac{\Delta}{a}$ must be greater than about 8 for errors of less than $1 \%$.
6. But, for the extended thin-wire kernel approximation, the radius of the wire can be increased for modeling large-diameter conductors, up to $\frac{\Delta}{a}=2$ for the same accuracy as the thin-wire kernel approximation.
7. If the distance between the ends of two segments is greater than about $1 E-3$ times the length of the shortest segment, NEC will not allow the current to flow from one segment to other.
8. Identical coordinates should be used for connected segment ends.
9. The end of one wire must be connected to the junction of two segments on another wire, and not to the mid-point of a single segment.
10. Large changes in radius between the two adjacent connected wires should be avoided. The change in radius between adjacent segments should generally be limited to a factor of two or less. It is also important that the largest radius not violate guidelines (5) and (6), in regard to the radius versus segment length.
11. A segment is required at each point where a network connection or a voltage source is located.
12. Any changes in segment length between two adjacent connected wires should be limited to a factor of $2: 1$ or less. Very long and straight wires may be modeled using tapered segment lengths (with the " GC " card), as long as the lengths of two adjacent scgments are held to a ratio of $2: 1$ or less.

## III. DESCRIPTION OF ANTENNA NUMERICAL MODELS

## A. HALF-WAVELENGTH HORIZONTAL DIPOLE

Figure 5 shows the configuration of the antenna. The results of this configuration for different frequencies and different types of ground can be used as a reference for comparison to other configurations. Generally speaking, the radiation patterns (elevation) show that this configuration is good for Near Vertical Incident Skywave (NVIS - high elevation angle radiation) communications, but it may also provide some ground wave (low elevation angle radiation) vertically polarized communications.

In Figure 6a the height of the antenna is close to one half-wavelength. For fair ground, since the image is not exactly of equal amplitude and opposite phase, there is not a perfect null at $\theta=0$. The azimuth pattern at $\theta=45$ degrees is shown in Figure 7. This antenna provides medium and long range communications. In Figure $6 b$ the height of the antenna is now close to two wavelengths with a near out of phase condition giving a maximum at $\theta=0$ and more lobes at this higher frequency ( 14.2 MHz ). It favors NVIS, medium, and relatively poor long range communications compared to same antenna at 3.8 MHz . Figure $S$ shows the azimuth pattern of this antenna at $\theta=43 \mathrm{de}$ grees. The four-wavelength high dipole provides good medium and long range communications as seen in Figure 6 c . The azimuth pattern of the same antenna is given in Figure 9.

The horizontally polarized gain is dominant over the vertically polarized gain in the broadside direction as seen in Figures 7, 8, and 9. These figures also show that this antenna is very good for skywave omnidirectional use because total gains of the antenna for different frequencies have a circular shape in the azimuth piane, especially for high frequenries (see Figures 8 and 9).

## B. QUARTER-WAVELENGTH SLOPING WIRE

The configuration of the quarter-wavelength sloping wire is in Figure 10. The resuits show that radiation patterns of a quarter-waveiength sioping wire are more directive than those of a half-wavelength horizontal dipole. But in some cases, the main lobe direction may not be in the sloping (desired) direction due to the antenna height, frequency, and top angles.

## half-WAVELENijth HORIZONTALLY POLARIZED DIPOLE



Figure 5. The half-wavelength horizontal dipole


Figure 6. The elevation patterns of the half-wavelength horizontal dipole: (a) Fr $=3.8 \mathrm{MHz}$ (b) $\mathrm{Fr}=14.2 \mathrm{MHz}$ (c) $\mathrm{Fr}=28.5 \mathrm{MHz}$

HOR.DIP. $\mathrm{H}=36.576 \mathrm{M}=120^{\prime} \mathrm{FR}=3.8 \mathrm{MHZ} \mathrm{L}=\mathrm{L} A M B D A / 2$ AZIMUTH PAT. $E P S=10, S 1 G=.003$ THETA $=45$


Figure 7. The azimuth pattern of the half-wavelength horizontal dipole: Antenna is 120 ft . high and frequency is 3.8 MHz


Figure 8. The azimuth pattern of the half-wavelength horizontal dipole: Antenna is 120 ft . high and frequency is 14.2 MHz


Figure 9. The azimuth pattern of the half-wavelength horizontal dipole: Antenna is 120 ft . high and frequency is 28.5 MHz

## QUARTER-WAVELENGTH SLOPING WIRE

- 30 AND 45 DEGREES TOP ANGLES (TA ).
- $50^{\circ}$ A.ND $90^{\circ} \mathrm{HIGH}$ ( H ).
- $4^{\prime}$ GROLND ROD.
- CONNECTED TOWER.
- FEED AT TOP.


Figure 10. The quarter-wavelength sloping wire

Figures 11 c and $\mathrm{d}, 12 \mathrm{a}$ and b , and 13 c and d show elevation patterns which have main lobes in the opposite direction of sloping (undesired) for frequencies of 28.5, 21.3, and 7.2 MHz respectively. From these figures, it can be seen that medium- and longrange communications can be provided and higher frequencies of HF band give multilobe radiation patterns. The height of the antenna, frequency, and top angle affect the side lobe levels.

In addition, radiation patterns of this configuration are more directive than those of a horizontal dipole in the direction the antenna slopes as seen in Figure 14.

## C. HALF-WAVELENGTH SLOPING DIPOLE

Figure 15 shows the configuration of the antenna. This configuration has a more directive pattern than the quarter-wavelength sloping wire. In general, the effects of height, frequency, and top angle are similar to those observed for the quarier-wavelength sloping wire.

Radiation patterns in Figure 16 show that large top angles produce small side lobes in the direction opposite of the slope. The vertically polarized gain is maximum in the sloping direction as seen in the azimuth pattern (Figure 17).

## D. HALF-WAVELENGTH INVERTED VEE DIPOLE

The configuration of the antenna is shown in Figure 18. Construction limitations restrict this antenna to a tower that is not electrically connected to the antenna and the angle between each leg and tower to be a maximum of 45 degrees. In addition, the distance between the end of each leg and the ground should not exceed 10 ft .

Figure 19 shows three elevation patterns of this configuration for frequencies of 3.8, 14.2, and 28.5 MHz and a 120 ft antenna. By comparing Figures 19 a and 23 , it can be seen that the inverted vee dipole provides radiation that is more directive than for a monopole antenna. This antenna also provides medium range as well as long range communication.

Increasing the frequency results in more gain for a 120 ft high antenna as seen in Figure 19. The elcvation patterns for frequencies of $3.8,14.2$, and 28.5 MHz with a 35 ft high antenna are in Figure 20. A comparison of Figures 19 and 20 shows that more gain is obtained by increasing frequency rather than by inctedsing the height of the antenna.

The azimuth pattern of the 35 ft high inverted vee dipole at a frequencr of 3.8 MHz is in Figure 21. This pattern is vertically polarized in the direction of the antenna.


Figure 11. The elevation patterns of the sloping wire for 28.5 MHz : (a) $T A=45$ degrees, $\mathrm{H}=50 \mathrm{ft}$. (b) $\mathrm{TA}=30$ degrees, $\mathrm{H}=50 \mathrm{ft}$. (c) $\mathrm{TA}=45$ degrees, $\mathrm{H}=90 \mathrm{ft}$. (d) $\mathrm{TA}=30$ degrees, $\mathrm{H}=90 \mathrm{ft}$.
WL/A SLP.WIRE.WITH CONNECTED TOWER AND 4 ' GR.ROD TAE $\angle 5$ EL.PAT, $E P S=10.51 C=.003 \quad\left[R=21.3 \mathrm{MHZ} H=50^{\circ}=15.24 \mathrm{M}\right.$

(a)
WL/ 4 SLP.WIRC.WITH CONNECTED IOWER AND $A^{\prime}$ GR.ROD TA $=30$ EL.PAT. $E P S=10, S 16=.003 \quad$ R $=21,3 \mathrm{MHZ} \mathrm{H}=50^{\prime}=15.24 \mathrm{M}$

(b)

WLA SUP.WIRE.WTH CONUECTEO TOWER AND 4 ' GR.ROD TA= 13 ELPAT, $E P S=10,51 G \pi, 003$ FR $=21.3 \mathrm{MHZ} \mathrm{H}=1 \mathrm{O}=27.432 \mathrm{M}$

(c)

WL/A SLP. WHRE. WITH CONNECTED TOWER AND $L^{\prime} G R . R O D ~ T A=30$ ELPAI. $\left[P S=10, S 1 G=.003 \quad\right.$ RR $=21.3 \mathrm{MHZ} \mathrm{H}=90^{\circ}=27.432 \mathrm{M}$

(d)
$\mathrm{TA}=\mathrm{TOP} \mathrm{ANGLE}$
$H=$ HEIGHT OF THE ANTENNA FROM THE GROUND


Figure 12. The elevation patterns of the sloping wire for 21.3 MHz : (a) $\mathrm{TA}=45$ degrees, $\mathrm{H}=50 \mathrm{ft}$. (b) $\mathrm{TA}=30$ degrees, $\mathrm{H}=50 \mathrm{ft}$. (c) $\mathrm{TA}=45$ degrees, $H=90 \mathrm{ft}$. (d) $\mathrm{TA}=30$ degrees, $\mathrm{H}=90 \mathrm{ft}$.


Figure 13. The elevation patterns of the sloping wire for 7.2 MHz : (a) $\mathrm{TA}=45$ degrees, $H=50 \mathrm{ft}$. (b) $T A=30$ degrees, $H=50 \mathrm{ft}$. (c) $T A=45$ degrees, $\mathrm{H}=90 \mathrm{ft}$. (d) $\mathrm{TA}=30$ degrees, $\mathrm{H}=90 \mathrm{ft}$.


Figure 14. The azimuth pattern of the quarter-wavelength sloping wire

## HALF-WAVELENGTH SLOPING DIPOLE

- 30 AÑ 45 DEGREES TOP ANGLES (TA)
- $50^{\circ}$ A.ND $90^{\circ} \mathrm{HIGH}$
- DETACHED TOWER
- CENTER FEED
- 4' Ground rod


Figure 15. The half-wavelength sloping dipole


Figure 16. The elevation patterns of the half-wavelength sloping dipole: (a) $T A=30$ degrees, $H=50 \mathrm{ft}$. (b) $\mathrm{TA}=45$ degrees, $\mathrm{H}=50 \mathrm{ft}$. (c) $\mathrm{TA}=30$ degrees, $\mathrm{H}=90 \mathrm{ft}$. (d) $\mathrm{TA}=45$ degrees, $\mathrm{H}=90 \mathrm{ft}$. and the frequency is 28.5 MHz for all patterns.

WL/2 SLOPING DIPOLE WITH DETACHED TOWER AND 4' GROUND ROD AZIMUTH PAT. EPS $=10, S I G=.003$ FR=28.5MHZ THETA=23


Figure 17. The azimuth pattern of the half-wavelength sloping dipole: $T A=45$ degrees, $\mathrm{H}=50 \mathrm{ft}$.

## HALF-WAVELENGTH INVERTED VEE DIPOLE WITH A DETACHED TOWER

HEIGHTS (ft.)

- 25
- 35
- 50
- 90
- 120


$$
\text { THETA }=90.00 \mathrm{PH}=60.00 \mathrm{ETA}=90.00
$$

Figure 18. The half-wavelength inverted vee dipole.


Figure 19. The elevation patterns of the 120 ft . high inv. vee dipole: (a) $\mathrm{Fr}_{\mathrm{r}}=3.8$ MHz (b) $\mathrm{Fr}=14.2 \mathrm{MHz}$ (c) $\mathrm{Fr}=28.5 \mathrm{MHz}$

## E. QUARTER-WAVELENGTH MONOPOLE WITH A 4 FOOT GPOUND ROD

Figure 22 shows the configuration of the antenna with insulated supporting wires and a 4 ft ground rod. The elcvation and azimuth patterns of this configuration are the same typical monopole radiation pattern shape as seen in Figures 23 and 24 respectively.

Its low take-off angle provides long distance skywave communications, but it has poor NVIS performance due to lower gain at the high elevation angles.

## F. QUARTER-WAVELENGTH MONOPOLE WITH RADIAL WIRES

## 1. Wires buried 2 inches deep ( 4,15 , and 30 wires)

The configurations of the antenna with 4 and 15 radial wires buried ? inches deep are in Figure 25. Figure 26 shows elevation and azimuth patterns of the 15 radial wire configuration. The shape of the radiation patterns were not effected by changing the frequency or any other antenna parareter such as the number of radials and type of ground system. The effects of these parameters are related to gain of the antenna.

The relative radiated power versus frequency (HF band) for different numbers of radial wires can be seen in Figure 27. It should be noted that higher frequencies produce more power as the number of radial wires increases.
2. Wires elevated $0.08 \%$ high ( 4,15 , and 30 wires)

Figure 28 shows the configurations of the antenna with 4 and 15 radial wires elevated $0.08 i$ high. Elevation and azimuth patterns of this antemna-for 15 radial wires can be seen in Figure 29.

The relative power versus frequency (HF band) for different number of elevated radial wires was plotted in Figure 30. This configuration witl: 4 radial wires produces more power than the same configuration with 15 and 30 radial wires. In addition, higher frequencies produce more power as the number of radial wires decreases.


Figure 20. The elevation patterns of the 35 ft . high inv, vee dipole: (a) $\mathrm{Fr}=3.8$ MHz (b) $\mathrm{Fr}=14.2 \mathrm{MHz}$ (c) $\mathrm{Fr}=28.5 \mathrm{MHz}$

INV. VEE DIP. $H=10.663 M=35^{\prime} F R=3.8 \mathrm{MHZ}$ L $\angle \mathrm{LAMBDA} / 2$ AZIMUTH PAT. $E P S=10, S I G=.003$ THETA $=45$


Figure 21. The azimuth pattern of the half-wavelength inverted vee dipole: Frequency is 3.8 MHz and the antenna is 35 ft high.

## QUARTER-WAVELENGTH MONOPOLE WITH A 4 FOOT GROUND ROD



Figure 22. The quarter-wavelength monopole with a 4 ft ground rod.


Figure 23. The elevation pattern of the quarter-wavelength monopole with a 4 ft ground rod.

## QUARTER WAVELENGTH MONOPOLE WITH $4^{\prime}$ GROUND ROD AZIMUTH PAT. $F R=3.8 \mathrm{MHZ}$ THETA=60



Figure 24. The azimuth pattern of the quarter-wavelength monopole with a 4 ft ground rod.

MONOFOLE WITH 4 RADIAL WIRES ( $2^{\prime \prime}$ BURIED) MONOPOLE WITH 15 RAOIAL WIRES ( 2 " BURILD)


THETA $=60.00$ PHI $=60.00$ EIA $=90.00$
(a)
(b)

Figure 25. The quarter-wavelength monopole with buried radial wires: (a) 4 wires (b) 15 wires


Figure 26. The radiation patterns of the monopole with buried radials: (a) Elevation pattern (b) Azimuth pattern


Figure 27. The performance curves of the buried radial wire system: Quarterwavelength monopole with radial wires buried 2 inches


MONOPOL.E WITH 15 RADIALS ( 08 Lambda ELEVATED )

THETA $=60.00 \mathrm{PH}:=60.00 \mathrm{ETA}=90.00$
(a)


Figure 28. The quarter-wavelength monopole with elevated radial wires: (a) 4 wires (b) 15 wires


Figure 29. The radiation patterns of the monopole with elevated radials: (a) Elevation pattern (b) Azimuth pattern


Figure 30. The performance curves of the elevated radial wire system: Quarterwavelength monopole with radial wires elevated 0.08 i high

## IV. CONCLUSIONS AND RECOMMENDATIONS

## A. CONCLUSIONS

Various configurations of monopole and dipole antennas have been studied at frequencies of $3.8,7.2,14.2,21.3$, and 28.5 MHz over fair (average) ground. All antennas were modeled using the Numerical Electromagnetics Code (NEC) with double precision accuracy. Specific observations are :

1. Radiation patterns of a half vavelength horizontal dipole may be used as a reference for other works. This antenna is good for NVIS communications; in addition, it may provide ground wave communications.
2. The quarter wavelength sloping wire and half wavelength sloping dipole provide more directional radiation than the half wavelength horizontal dipole. Antenna parameters, such as the frequency; height of the antenna, and top angle should be chosen to produce a main lobe in the desired direction.
3. A half-wavelength inverted vee dipole produces radiation that is more directive than that of a monopole antenna and provides medium- and long-range communications. More gain can be obtained by increasing frequency rather than by increasing the height of the antenna.
4. The quarter wavelength monopole provides good ground wave communications. The shywave does not depend on ground constants as much as the ground wave does, but it has poor NVIS performance.
5. The monopole with a ground rod is less effective than with a radial wire ground system in reducing the effect of linite ground on low-angle radiation.
6. A radial wire ground system is a good ground plane for a monopole. The followings are observations of radial wire ground systems:

- With fewer radial wires, the elevated radial wire ground system gives better results than the buried ground system (compare Figures 27 and 30).
- The increase in radiated power for a monopole with buried radial wires when the number of wires are between 4 and 15 is more than the increase between 15 and 30 wires (Figure 27).
- Higher frequencies show more radiated power for both buried and elevated radial wire ground sy:stems (Figures 27 and 30).

7. The effect of imperfect ground on the radiation pattern is less severe for horizontal antennas than for vertical antennas.

## B. RECOMMENDATIONS

Acditional studies are needed:

1. In this thesis, the antennas have been studied at frequencies of $3.8,7.2,14.2,21.3$,
and 28.5 MHz over fair ground. The work can be extended by doing more analysis at different frequencies in the HF band and over different types of ground.
2. Antenna types investigated were various configurations of monopoles and dipoles in this thesis. Other types of conventional antenna configurations shou'd also be studied.
3. New geometrical structures of wire antennas can be created and modelled based on the performance of antennas in this study.

## APPENDIX A. NPGNEC MAINFRAME (NEC-3) LIBRARY

A brief description of the programs which can be found in the NEC FORTRAN library are described below:

1. NECARY

A version of NEC designed for use with large arrays.
2. NecGs

A version of NEC which makes use of geometrical symmetry in order to simplify generation of monopole structures. It is quite useful for analysis of monopoles with radial wires and with top loading.
3. APG .IEC (…EC3)

The most current and capable version of NEC available at NPS. It is suitable for wires above and beneath the interface.
4. NPSNEC (. AEC 2 )

A mainframe implementation of $\mathrm{NEC2}$ (which is normally used on a PC).
5. PLOTDG

A ploting program that plots the geometry created by NEC geometry data cards. It is useful for checking these cards before submitting a job for processing.
6. PLOTAF

A program used to plot near fields in log or linear format.
7. PLOTDGLP

A program designed for plotting the data geometry on the laser printer for thesis use.
8. PlotidgTx

A program used for ploting the data geometry on a TEK61S display unit.
9. PLOTDG79

A program for ploting the data geometry on a 3279 terminal.
10. PLOTHSSD

A program designed for plotting radiation patterns of the sky and surface waves. The input must contain horizontal. vertical, and radial components. The output is a plot of all three components plus the total in dB. V, M.
11. PLOTHSW

A program similar to PLOTH3SD except the output is in V/M.
12. PLOTHNAB

This program plots surface wave data for azimuth patterns in mV.M.
15. PLOTXAB

This program plots sky and surface wave elevation patterns in mV, M.

## 14. PLOTRPHM

A program for ploting the horizontal. vertical, and total gain components of azimuth radiation patterns.

## 13. PLOTRPVM

A program like PLOTRPHM for plotting radiation patterns in the vertical plane for free space.
16. PLOTRPVE

A program like PLOTRPHM for plotting radiation patterns in the vertical plane for half space.
17. RPIMAKER

A program generating the NEC RP1 cards needed to get vertical plane surface wave data for plotting.
18. SOMNEC

A program generating the interpolation table when using the Sommerfeld Norton method for finite ground environments. It must be run prior to $N E C 2$ when the Sommerfeld, Norton ground option appears on a ground (GN) card; it requires epsilon, sigma, and frequency in MHz .

## 19. SOM.TX

A program similar to SO:M.NEC, but for use with NEC3.
The $\operatorname{NEC}$. Module library includes modules compiled from the above FORTRAN programs. RECO: < filename > must be typed to get the module from the MVS library into a form that can be run on V.M:C.MS.

## APPENDIX B. SAMPLE SESSION OF NEC

The following steps explain the NEC session process. It would vary depending on the particular circumtances and the type of problems.

## A. LOG ON

B. GET NECPROF RUNNING

Type NECPROF and enter.
Type IC:MS and enter.
Type NECPROF and enter.
The first entry of NECPROF is to start to NEC session ; the second one is to format the disk which will be used.

## C. CREATE DATA FILE

This should be done on the $B$ disk, but it is not necessary. To get into the $B$ disk use PF9.PF21 key, then use XEDIT to create a data file, for example, MWRW1 DATA B1 (see Volume II). It can then be run by using the PF2 or PF14 keys, or by typing the name of the program which will be run next to the data file in the $B$ disk file list. After the program run, the $B$ disk file list includes the following files:

MWRWI DATA BI
FILE FTOSF001 BI
MWRWI LISTING BI
MWRW1 PLOTDATA B1
It should be noted that to get to the abore display, it is necessary to exit from the old B disk file list display by using the PF3, PF15 key and then get back into it by using the PF9 PF21 kes.
D. EXECL゙IL HE CHOSEN PLOTTING PROGRAM

The plotting program to be used is determined by which display is needed. For example, if a horizontal azimuthal plot of the data is needed, PLOTRPHM is used by first typing RECO. PLOTRPH.M. Then, to display a horizontal azimuthal radiation pattern, PLOTRPHM is typed next to MWRWI PLOTDATA in the B disk file list. The result will appear either on the TEK618 display unit (if TEK618 was selected in the PLOTC.MD file) or as a DISSPLA METAFILE (if COMPRS option was selected in the PLOTC.MD file). If the second option was selected, the PF3 PF9 key should be used to see DISSPLA METAFILE which was just created. To send METACILE through the

DISSPLA plotting program, DISSPOP or THESPOP should be typed next to METAFILE in the B disk file list. This will produce a plot on the IBM 3800 laser printer.

## E. LISTING FILES

During the running of the program, a LISTING file is created. The listing shows the results of the calculations. It can be printed by typing PRINT next to the file name in the B disk file list. Normally this printout and a plot represent the output to be saved.

## F. LOGGING OFF

Before logging off, since the B disk is temporary, the files needed or necessary should be saved by sending them to the A disk. This is done by typing the CA next to a filename in the $B$ disk file list. To work with this file again, it can be sent to the $B$ disk by typing CB next to the filename in the A disk file list. After the necessary files have been saved, the session will be terminated by typing LOG. It is possible to get back to the ICMS without logging off.

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Denizalti Filosu K.ligi - Golcuk - KOCAELI - TURKEY
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Cameron Station
Alexandria. Virginia 22304-6145

RPO , 1, 121, 1500, 20, 0. 0, 0, 3, 0
RP0, $1,121,1500,10,0.0,0,3,0$
RPO, 1, 121, 1500,0,0.0,0,3,0
EN


CM GEOMETRY : QUARTER WAVELENGTH MONOPOLE
CM WITH QUARTER WAVELENGTH 4 RADIAL WIRES BURIED $2^{11}=.0508 \mathrm{M}$ DEEP
CM FREQUENCY : 7.2MHZ
$\begin{array}{ll}\text { CM } & \text { WAVELENGTH (FOR SKY WAVES) }\end{array}=41.66 \mathrm{M}$
CM WIRE : 非12 ( RADIUS R=. 010265M)
$C M$ GROUND $(0):$ EPSILON $=10 \quad$ SIGMA $=003$
CE
GW 2, 1, 0,0,0, . 2902,0,-.0508, . 010265
GW 3,9,.2902, 0, -. $0508,2.94178,0,-.0508, .010265$
GR 0,4
GW $1,10,0,0,0,0,0,10.4166, .010265$
GE 0
FR 0,0,0,0,7.2
GN 2,0,0,0,10,. 003
EX $0,1,1,01,1,0$

```
PL3,2,1,0
RP1,1,121,0,7.62,0.0,0,3,1609.3
PL3,2,2,0
RP1,1,121,0,7.62,0.0,0,3,1609.3
PLO,0,0,0
RPO,1,121,1500,80,0.0,0,3,0
RPO,1,121,1500,70,0.0,0,3,0
RPO,1,121,1500,60,0.0,0,3,0
RPO,1,121,1500,50,0.0,0,3,0
RPO,1,121,1500,40,0.0,0,3,0
RPO,1,121,1500,30,0.0,0,3,0
RPO,1,121,1500,20,0.0,0,3,0
RPO,1,121,1500,10,0.0,0,3,0
RPO,1,121,1500,0,0.0,0,3,0
EN
```



| CM GEOMETRY | QUARTER WAVELENGTH MONOPOLE |
| :---: | :---: |
| CM | WITH QUARTER WAVELENGTH 30 RADIAL WIRES |
| CM | BURIED $2^{\prime \prime}=.0508 \mathrm{M}$ DEEP |
| CM FREQUENCY | 7.2MHZ |
| CH | WAVELENGTH (FOR SKY WAVES) $=41.66 \mathrm{M}$ |
| CM | WAVELENGTH (FOR GROUND WAVES) $=11.785 \mathrm{M}$ |

```
CM WIRE : \#12 ( RADIUS R=. 010265M)
CM GROUND(0) : EPSILON \(=10 \quad\) SIGMA \(=.003\)
CE
GW 2,1, 0,0,0, . 2902,0, -. 0508, . 010265
GW 3,3, . \(2902,0, \cdots .0508,2.94178,0,-.0508, .010265\)
GR 0,30
GW 1,10, 0,0,0, 0,0,10.4166, . 010265
GE 0
FR 0,0,0,0,7.2
GN 2,0,0,0,10,. 003
EX \(0,1,1,01,1,0\)
PL3, 2, 1, 0
RP1, \(1,121,0,7.62,0.0,0,3,1609.3\)
PL3,2,2,0
RP1, 1. \(121,0,7.62,0.0,0,3,1609.3\)
PLO, 0,0,0
RPO, 1, 121, 1500, \(80,0.0,0,3,0\)
RPO, 1, 121, 1500, 70,0.0,0,3,0
RP0,1,121,1500,60,0.0,0,3,0
RPO, \(1,121,1500,50,0.0,0,3,0\)
RPO \(, 1,121,1500,40,0.0,0,3,0\)
RP0,1,121, 1500, \(30,0.0,0,3,0\)
RPO , 1, 121,1500, 20, 0.0,0,3,0
RPO \(, 1,121,1500,10,0.0,0,3,0\)
RPO \(1,121,1500,0,0.0,0 ; 3 ; 0\)
EN
\begin{tabular}{|c|}
\hline CM GEOMETRY : QUARTER WAVELENGTH MONOPOLE \\
\hline CM WITH QUARTER WAVELENGTH 4 RADIAL WIRES \\
\hline CM BURIED \(2^{\prime \prime}=.0508 \mathrm{M}\) DEEP \\
\hline CM FREQUENCY : 14.2 MHZ \\
\hline CM WAVELENGTH (FOR SKY WAVES) \(=21.167 \mathrm{M}\) \\
\hline CM WAVELENGTH (FOR GROUND WAVES) \(=6.459 \mathrm{M}\) \\
\hline CM WIRE : \#12 ( RADIUS \(\mathrm{R}=.010265 \mathrm{M}\) ) \\
\hline CM GROUND (0) : EPSILON = 10 SIGMA \(=003\) \\
\hline CE \\
\hline GW 2, 1, 0,0,0, . 1533, 0, -. 0508, .010265 \\
\hline GW 3,9, . \(1533,0,-.0508,1.60653,0,-.0508, .010265\) \\
\hline GR 0,4 \\
\hline GW 1, 10, 0, 0,0, 0,0,5.2816, . 010265 \\
\hline GE 0 \\
\hline FR 0,0,0,0,14.2 \\
\hline GN 2,0,0,0,10,.003 \\
\hline EX \(0,1,1,01,1,0\) \\
\hline PL3, 2, 1,0 \\
\hline RP1, \(1,121,0,7.62,0.0,0,3,1609.3\) \\
\hline PL3, 2, 2, 0 \\
\hline RP1, 1, 121, 0, 7. 62, 0.0,0,3,1609.3 \\
\hline PLO, 0,0,0 \\
\hline RP0,1,121, 1500,80,0.0,0,3,0 \\
\hline RPO, 1, 121, 1500, \(70,0.0,0,3,0\) \\
\hline RP0, 1, 121, 1500,60,0.0,0,3,0 \\
\hline \(\mathrm{RP} 0,1,121,1500,50,0.0,0,3,0\) \\
\hline RP0, 1, 121, 1500,40,0.0,0,3,0 \\
\hline \(\mathrm{RP} 0,1,121,1500,30,0.0,0,3,0\) \\
\hline RP0, 1, 121, 1500, \(20,0.0,0,3,0\) \\
\hline
\end{tabular}
```

```
RP0, 1, 121, 1500, 10, 0. 0, 0,3,0
RPO,1,121, 1500,0,0.0,0,3,0
EN
```

| CM GEOMETRY ：QUARTER WAVELENGTH MONOPOLE |
| :---: |
| CM WITH QUARTER WAVELENGTH 15 RADIAL WIRES |
| CM BURIED $2^{\prime \prime}=$ ． 0508 M DEEP |
| CM FREQUENCY ：14．2MHZ |
| CM WAVELENGTH（FOR SKY WAVES）$=21.1267 \mathrm{M}$ |
| CM WAVELENGTH（FOR GROUND WAVES）$=6.459 \mathrm{M}$ |
| CM WIRE ：$⿰ ⿰ 三 丨 刃 丨 12$（ RADIUS $\mathrm{R}=.010265 \mathrm{M}$ ） |
| CM $\operatorname{GROUND}(0):$ EPSILON $=10 \quad$ SIGMA $=.003$ |
| CE |
| GW 2，1，0，0，0，． $3183,0,-.0508, .010265$ |
| GW 3，4，． $3183,0,-.0508,1.6107,0,-.0508, .010265$ |
| GR 0，15 |
| GW 1，5，0，0，0，0，0，5．2816，． 010265 |
|  |
| FR 0，0，0，0，14．2 |
| GN 2，0，0，0，10，．003 |
| EX 0，1，1，01，1，0 |
| PL3，2，1，0 |
| RP1，1，121，0，7．62，0．0，0，3，1609． 3 |
| PL3，2，2，0 |
| RP1，1，121，0，7．62， $0.0,0,3,1609.3$ |
| PLO， $0,0,0$ |
| RPO，1，121，1500，80，0．0，0，3，0 |
| RP0，1，121，1500， $70,0.0,0,3,0$ |
| RPO，1，121，1500， $60,0.0,0,3,0$ |
| RPO，1，121，1500， $50,0.0,0,3,0$ |
| RP0，1，121，1500，40，0．0，0，3，0 |
| RP0，1，121，1500， $30,0.0,0,3,0$ |
| RP0，1，121，1500， $20,0.0,0,3,0$ |
| RP0，1，121，1500，10，0．0，0，3，0 |
| RP0，1，121，1500， $0,0.0,0,3,0$ |
| EN |

CM GEOMETRY : QUARTER WAVELENGTH MONOPOLE
CM WITH QUARTER WAVELENGTH 30 RADIAL WIRES
CM BURIED $2^{\prime \prime}=.0508 \mathrm{M}$ DEEP
CM FREQUENCY : 14. 2 MHZ
$\begin{array}{ll}\mathrm{CM} & \text { WAVELENGTH (FOR SKY WAVES) } \\ \mathrm{CM} & =21.1267 \\ \text { WAVELENGTH (FOR GROUND WAVES) } & =6.459 \mathrm{M}\end{array}$
$\begin{array}{lll}\text { CM } & \text { WAVELENGTH (FOR SKY WAVES) } & =21.1267 M \\ C M & \text { WAVELENGTH (FOR GROUND WAVES) } & =6.459 \mathrm{M}\end{array}$
CM WIRE : \#12 ( RADIUS R=.010265M)
CM GROUND(0) : EPSILON $=10 \quad$ SIGMA $=.003$
CE
GW 2, 1, 0,0,0, . 3183, 0, -. 0508, . 010265
GW 3,4,. $3183,0,-.0508,1.6107,0,-.0508, .010265$
GR 0,30
Giv $1,5,0,0,0,0,0,5.2816, .010265$
GE 0
FR $0,0,0,0,14.2$
GN 2,0,0,0,10,. 003
EX $0,1,1,01,1,0$
PL3, 2, 1,0

```
RP1,1,121,0,7.62,0.0,0,3,1609.3
PL3,2,2,0
RP1,1,121,0,7.62,0.0,0,3,1609.3
PLO,0,0,0
RP0,1,121,1500,80,0.0,0,3,0
RPO,1,121,1500,70,0.0,0,3,0
RPO,1,121,1500,60,0.0,0,3,0
RPO,1,121,1500,50,0.0,0,3,0
RPO,1,121,1500,40,0.0,0,3,0
RPO,1,121,1500,30,0.0,0,3,0
RPO,1,121,1500,20,0.0,0,3,0
RPO,1,121,1500,10,0.0,0,3,0
RPO,1,121,1500,0,0.0,0,3,0
EN
```

CM GEOMETRY : QUARTER WAVELENGTH MONOPOLE
CM WITH QUARTER WAVELENGTH 4 RADIAL WIRES
BURIED $2^{\prime \prime}=.0508 \mathrm{M}$ DEEP
M FREQUENCY : 21.3NHZ
WAVELENGTH (FOR SKY WAVES) $=14.0845 \mathrm{M}$
WAVELENGTH (FOR GROUND WAVES) $=4.385 M$
CN
$\begin{array}{ll}C M \text { WIRE } & : \# 12(R A D I U S ~ R=.010265 M) \\ C M ~ G R O U N D(0): ~ E P S I L O N ~\end{array}=10 \quad$ SIGMA $=.003$
CE
GW 2, 1, $0,0,0, .097138,0,-.0508, .010265$
GW $3,9, .097138,0,-.0508,1.083718,0, \cdots .0508, .010265$
GR 0,4
GW $1,10,0,0,0,0,0,3.5211, .010265$
GE 0
FR $0,0,0,0,21.3$
GN $2,0,0,0,10, .003$
EX $0,1,1,01,1,0$
PL3,2,1,0
RP1, 1, 121, 0, 7. 62, 0. 0, 0, 3, 1609.3
PL3,2,2,0
RP1,1, 121,0,7.62,0.0,0,3,1609.3
PLO,0,0,0
RP0, 1, 121, $1500,80,0.0,0,3,0$
$\mathrm{RPO}, 1,121,1500,70,0.0,0,3,0$
$\operatorname{RPO}, 1,121,1500,60,0.0,0,3,0$
RPO , 1, 121, 1500, 50,0.0,0,3,0
RPO, $1,121,1500,40,0.0,0,3,0$
RPO, 1, 121, 1500, 30,0.0,0,3,0
RPO, $1,121,1500,20,0.0,0,3,0$
RPO, 1, 121, 1500, 10,0.0,0,3,0
RP0, $1,121,1500,0,0.0,0,3,0$
EN


```
CM GROUND(0) : EPSILON = 10 SIGMA=. }00
CE
GW 2,1, 0,0,0,. 2694,0, ..0508,.010265
GW 3,3,.2694,0,-.0508, 1.0915,0,-.0508,.010265
GR 0,15
GW 1,10, 0,0,0, 0,0,3.5211,.010265
GE 0
FR 0,0,0,0,21.3
GN 2,0,0,0,10,.003
EX 0,1,1,01,1,0
PL3,2,1,0
RP1,1,121,0, 7. 62,0.0,0,3, 1609.3
PL3,2,2,0
RP1,1,121,0,7.62,0.0,0,3,1609.3
PLO,0,0,0
RPO,1,121,1500,80,0.0,0,3,0
RPO,1,121,1500,70,0.0,0,3,0
RPO,1,121,1500,60,0.0,0,3,0
RPO,1,121,1500,50,0.0,0,3,0
RPO,1,121,1500,40,0.0,0,3,0
RPO,1,121,1500,30,0.0,0,3,0
RP0,1,121,1500,20,0.0,0,3,0
RPO,1,121,1500,10,0.0,0,3,0
RPO,1,121,1500,0,0.0,0,3,0
EN
```



RP0, 1, 121, 1500,0,0.0,0,3,0
EN


```
PL3,2,2,0
RP1,1,121,0,7.62,0.0,0,3,1609.3
PLO,0,0,0
RPO,1,121,1500,80,0.0,0,3,0
RP0,1,121,1500,70,0.0,0,3,0
RPO,1,121,1500,60,0.0,0,3,0.
RPO, 1,121,1500,50,0.0,0,3,0
RPO,1,121,1500,40,0.0,0,3,0
RPO,1,121,1500,30,0.0,0,3,0
RPO,1,121,1500,20,0.0,0,3,0
RPO,1,121, 1500,10,0,0,0,3,0
RPO,1,121,1500,0,0.0,0,3,0
EN
```

CM GEOMETRY : QUARTER WAVELENGTH MONOPOLE
CM
$\begin{array}{ll}\text { CM } & \text { WITH QUARTER WAVELENGT } \\ \text { CM } & \text { BURIED } 2^{11}=.0508 M \text { DEEP }\end{array}$
CM FREQUENCY : 28.5MHZ
$C M$ WAVELENGTH (FOR SKY WAVES) $=10.5263 \mathrm{M}$
CM WAVELENGTH (FOR GROUND WAVES) $=3.299 \mathrm{M}$
CM WIRE : \#12 ( RADIUS R=.010265M)
CM GROUND (0) : EPSILON $=10 \quad$ SIGNA $=003$
CE
GW $2,1,0,0,0, .1998,0,-.0508, .010265$
GW 3, 3, . 1998, 0, -. 0508, . 8183,0,-.0508, . 010265
GR 0,30
GW $1,10,0,0,0,0,0,2.6315, .010265$
GE 0
FR $0,0,0,0,28.5$
GN 2,0,0,0,10,.003
EX $0,1,1,01,1,0$
PL3, 2, 1,0
RP1, $1,121,0,7.62,0.0,0,3,1609.3$
PL3,2,2,0
RP1, $1,121,0,7.62,0.0,0,3,1609.3$
PLO, 0,0,0
$\operatorname{RPO}, 1,121,1500,80,0.0,0,3,0$
RPO, 1, 121, 1500, $70,0.0,0,3,0$
$\mathrm{RPO}, 1,121,1500,60,0.0,0,3,0$
RPO, $1,121,1500,50,0.0,0,3,0$
RPO , 1, 121, 1500, 40,0.0,0,3,0
RPO, $1,121,1500,30,0.0,0,3,0$
RPO , 1, 121, 1500, 20,0.0,0,3,0
KPO, 1, 121, 1500, $10,0.0,0,3,0$
RPO $1,121,1500,0,0.0,0,3,0$
EN
CM GEOMETRY : QUARTER WAVELENGTH MONOPOLE
CM WITH QUARTER WAVELENGTH 4 RadiÀ Wires
CM ELEVATED . O8LAMBDA $=6.3158 \mathrm{M}$
CM FREQUENCY : 3.8MHZ
CM WAVELENGTH (FOR SKY WAVES) $=78.9473 \mathrm{M}$
CM WAVELENGTH (FOR GROUND WAVES) $=18.939 \mathrm{M}$
CM WIRE : \#12 ( RADIUS $R=.010265 \mathrm{M}$ )
CM GROUND (0) : EPSILON $=10 \quad$ SIGMA $=.003$

```
CE
GW 1,10, 0,0,6.3158, 19.7368,0,6.3158,.010265
GR 0,4
GW 2,10, 0,0,6.3158, 0,0,26.0526, .010265
GW 3,1, 0,0,6.3058, 0,0,0,.010265
GW 4,1, 0,0,0, 0,0,-1.2192,.010265
GE O
FR 0,0,0,0,3.8
GN 2,0,0,0,10,.003
EX 0,2,1,01,1,0
PL3,2,1,0
RP1,1,121,0,7.62,0.0,0,3,1609.3
PL3,2,2,0
RP1,1,121,0,7.62,0.0,0,3,1609.3
PLO,0,0,0
RPO,1,121,1500,80,0.0,0,3,0
RPO,1,121,1500,70,0.0,0,3,0
RPO,1,121,1500,60,0.0,0,3,0
RPO,1,121,1500,50,0.0,0,3,0
RPO,1,121,1500,40,0.0,0,3,0
RPO,1,121,1500,30,0.0,0,3,0
RPO,1,121,1500,20,0.0,0,3,0
RP0,1,121,1500,10,0.0,0,3,0
RPO ,1,121,1500,0,0.0,0,3,0
EN
CM GEOMETRY : QUARTER WAVELENGTH MONOPOLE
CM
CM
                                    WITH QUARTER WAVELENGTH 15 RADIAL WIRES
                                    ELFVATED . O8LAMBDA=5.3158M
CM FREQUENCY : 3.8MHZ
CM WAVELENGTH (FOR SKY WAVES) = 78.9473M
CM WAVELENGTH (FOR GROUND WAVES) = 18.939M
CM WIRE : #12 ( RADIUS R=.010265M)
CM GROUND(0) : EPSILON = 10 SIGMA=.003
CE
GW 1,10, 0,0,6.3158, 19.7368,0,6.3158, . }01026
GR 0,15
GW 2,10, 0,0,6.3158, 0,0,26.0526,.010265
GW 3,1, 0,0,6.3058, 0,0,0,.010265
GW 4,1, 0,0,0, 0,0,-1.2192,.010265
GE 0
FR 0,0,0,0,3.8
GN 2,0,0,0,10,.003
EX 0,2,1,01,1,0
PL3,2,1,0
RP1,1,121,0,7.62,0.0,0,3,1609.3
PL3,2,2,0
RP1,1,121,0,7. 62,0.0,0,3,1609.3
PLO,0,0,0
RPO,1,121,1500,80,0.0,0,3,0
RP0,1,121,1500,70,0.0,0,3,0
RP0,1,121,1500,60,0.0,0,3,0
RP0,1,121,1500,50,0.0,0,3,0
RP0,1,121,1500,40,0.0,0,3,0
RP0,1,121,1500,30,0.0,0,3,0
RP0,1,121,1500,20,0.0,0,3,0
```

RPO , 1, 121, $1500,10,0.0,0,3,0$
RPO, 1, 121, 1500, 0,0.0,0,3,0
EN

| CM GEOMETRY : QUARTER WAVELENGTH MONOPOLE |
| :---: |
| CM WITH QUARTER WAVELENGTH 30 RADIAL WIRES |
| CM ELEVATED . O8LAMBDA=6.3158M |
| CM FREQUENCY : 3.8MHZ |
| CM WAVELENGTH (FOR SKY WAVES) $=78.9473 \mathrm{M}$ |
| CM WAVELENGTH (FOR GROUND WAVES) $=18.939 \mathrm{M}$ |
| CM WIRE : \#112 ( RADIUS $\mathrm{R}=.010265 \mathrm{M}$ ) |
| CM $\operatorname{GROUND}(0): \operatorname{EPSIL} O N=10 \quad$ SIGMA $=.003$ |
| CE |
| GW 1,5, 0,0,6.3158, 19.7368,0,6.3158, . 010265 |
| GR 0,30 |
| GW 2,10, 0,0,6.3158, 0,0,26.0526, . 010265 |
| GW 3,1, 0,0,6.3058, 0,0,0, . 010265 |
| GW 4, 1, 0,0,0, 0,0,-1.2192,.010265 |
|  |
| FR 0,0,0,0,3.8 |
| GN $2,0,0,0,10, .003$ |
| EX $0,2,1,01,1,0$ |
| PL3, $2,1,0$ |
| RP1, 1, 121, 0, 7. 62, 0.0, 0, 3,1609.3 |
| PL3, 2, 2,0 |
| RP1, 1, 121, $0,7.62,0.0,0,3,1609.3$ |
| PLO, 0,0,0 |
| RPO, 1, 121, 1500, $80,0.0,0,3,0$ |
| RPO $, 1,121,1500,70,0.0,0,3,0$ |
| RP0, 1, 121, 1500,60, $0.0,0,3,0$ |
| RP0, 1, 121, 1500,50, 0.0,0,3,0 |
| RPO, 1, 121,1500,40,0.0,0,3,0 |
| RPO, 1, 121, 1500, $30,0.0,0,3,0$ |
| RPO, 1, 121, 1500,20,0.0,0,3,0 |
| RPO, 1,121,1500,10,0.0,0,3,0 |
| RPO, 1, 121, 1500, $0,0.0,0,3,0$ |
| EN |

CH GEOMETRY : QUARTER WAVELENGTH MONOPOLE


$$
\text { EX } 0,2,1,01,1,0
$$

PL3,2,1,0
RP1, 1, 121,0,7.62,0.0,0,3,1609.3
PL3, 2,2,0
RP1,1,121,0,7.62, 0.0,0,3,1609.3
PLO, 0,0,0
RPO, $1,121,1500,80,0.0,0,3,0$
RPO, 1, 121, 1500, 70,0.0,0,3,0
RPC, 1, 121, 1500, 60,0.0,0,3,0
RPO,1,121,1500,50,0.0,0,3,0
RPO, 1, 121,1500,40,0.0,0,3,0
RP0,1,121,1500,30,0.0,0,3,0
RPO, 1,121,1500,20,0.0,0,3,0 RPO, 1, 121,1500,10,0.0,0,3,0
RP0, 1, 121, 1500, 0, 0. 0, 0,3,0
EN



```
RPO, 1, 121, 1500,50,0.0,0,3,0
RPO, 1, 121, 1500, 40,0.0,0,3,0
RPO , 1, 121, 1500, 30,0.0,0,3,0
RP0, 1, 121, 1500, 20,0.0,0,3,0
RPO, 1, 121, 1500,10,0.0,0,3,0
RPO \(1,121,1500,0,0.0,0,3,0\)
EN
```

|  | CM GEOMETRY : QUARTER WAVELENGTH MONOPOLE |
| :---: | :---: |
|  | CM WITH QUARTER WAVELENGTH 15 RADIAL WIRES |
|  | CM ELEVATED . O8LAMBDA $=1.6901 \mathrm{M}$ |
|  | CM FREQUENCY : 14.2 MHZ |
|  | CM WAVELENGTH (FOR SKY WAVES) $=21.1268 \mathrm{M}$ |
|  | CM WAVELENGTH (FOR GROUND WAVES) $=6.459 \mathrm{M}$ |
|  | CM WIRE : \#12 ( RADIUS $\mathrm{R}=.010265 \mathrm{M}$ ) |
|  | CM GROUND (0) : EPSILON = 10 SIGMA $=.003$ |
|  | CE |
|  | GW $1,10,0,0,1.6901,5.2817,0,1.6901, .010265$ |
|  | GR 0,15 |
|  | GW 2, 10, 0,0,1.6901, 0,0,6.9718, 010265 |
|  | GW 3,1, 0,0,1.6801, 0,0,0, .010265 |
|  | GW 4,3, 0,0,0, 0,0,-1. 2192, . 010265 |
|  |  |
|  | FR 0,0,0,0,14.2 |
|  | GN 2,0,0,0,10,.003 |
|  | EX $0,2,1,01, \therefore, 0$ |
|  | PL3,2,1,0 |
|  | RP1, 1, 121, 0, $7.62,0.0,0,3,1609.3$ |
|  | PL3, $2,2,0$ |
|  | RP1, 1, 121, 0, 7. 62, 0.0, 0, 3, 1609.3 |
|  | PLO, $0,0,0$ |
|  | RP0, 1, 121, 1500, $80,0.0,0,3,0$ |
|  | $\mathrm{RP} 0,1,121,1500,70,0.0,0,3,0$ |
|  | RPO, 1, 121, 1500,60,0.0,0,3,0 |
|  | RP0,1,121,1500,50,0.0,0,3,0 |
|  | RPO, 1, 121, 1500,40,0.0,0,3,0 |
|  | RPO, 1, 121, 1500, $30,0.0,0,3,0$ |
|  | RP0, 1, 121, 1500, $20,0.0,0,3,0$ |
|  | RP0, 1, 121,1500,10,0.0,0,3,0 |
|  | RPO, 1, 121, 1500, $0,0.0,0,3,0$ |
|  | EN |



GW 4,3, 0,0,0, 0,0,-1.2192, . 010265
GE 0
FR 0,0,0,0,i4. 2
GN 2,0,0,0,10,. 003
EX $0,2,1,01,1,0$
PL3,2,1,0
RP1,1,121,0, 7. 62,0.0,0,3,1609. 3
PL3,2,2,0
RP1, $1,121,0,7.62,0.0,0,3,1609.3$
PLO, 0,0,0
RP0, 1, 121, 1500, $80,0.0,0,3,0$
RP0,1,121,1500,70,0.0,0,3,0
RPO, 1, 121, 1500,60,0.0,0,3,0
RPO, 1,121, 1500,50,0.0,0,3,0
RPO, 1, 121, 1500,40,0.0,0,3,0
RPO $1,121,1500,30,0.0,0,3,0$
RP0, 1, 121, 1500, 20,0.0,0,3,0
RP0,1,121,1500,10,0.0,0,3,0
RP0, 1, 121, 1500, 0, 0.0,0,3,0
EN

CM GEOMETRY : QUARTER WAVELENGTH MONOPOLE
CM WITH QUARTER WAVELENGTH 4 RADIAL WIRES
CM ELEVATED . O8LAMBDA $=1.1268 \mathrm{M}$
CM FREQUENCY
21.3 MHz

CM
CN WAVELENGTH (FOR SKY WAVES) $=14.0845 \mathrm{M}$ WAVELENGTH (FOR GROUND WAVES) $=4.385 \mathrm{M}$
CM WIRE : \#12 (RADIUS $\mathrm{R}=.010265 \mathrm{M}$ )
CM $\operatorname{GROUND}(0): \operatorname{EPSILON}=10 \quad$ SIGMA $=.003$
CE
GW $1,10,0,0,1.1268,3.5211,0,1.1268, .010265$
GR 0,4
GW 2,10, 0,0,1.1268, 0,0,4.6479, . 010265
GW 3,1, $0,0,1.1168,0,0,0, .010265$
GW 4,4, 0,0,0, 0,0,-1.2192, . 010265
GE 0
FR 0,0,0,0,21.3
GN $2,0,0,0,10, .003$
EX $0,2,1,01,1,0$
PL3, 2, 1, 0
RP1, 1, 121, 0, 7. 62, 0.0, 0, 3, 1609. 3
PL3, 2, 2,0
RP1, $1,121,0,7.62,0.0,0,3,1609.3$
PLO, $0,0,0$
RPO , 1, 121, 1500, 80, 0.0,0,3,0
RPO $1,121,1500,70,0.0,0,3,0$
RPO, 1, 121, 1500,60,0.0,0,3,0
RPO,1,121,1500,50,0.0,0,3,0
RPO, 1, 121, 1500, 40,0.0,0,3,0
RPO , 1, 121, 1500, 30, 0.0,0,3,0
RP0, 1, 121, 1500, 20,0.0,0,3, 0
RP0, 1, 121, 1500, 10,0.0,0,3,0
RP0, $1,121,1500,0,0.0,0,3,0$
EN


```
PLO,0,0,0
RPO,1,121,1500,80,0.0,0,3,0
RPO,1,121,1500,70,0.0,0,3,0
RPO,1,121,1500,60,0.0,0,3,0
RP0,1,121,1500,50,0.0,0,3,0
RPO,1,121,1500,40,0.0,0,3,0
RPO,1,121,1500,30,0.0,0,3,0
RPO,1,121,1500,20,0.0,0,3,0
RPO,1,121,1500,10,0.0,0,3,0
RPO,1,121,1500,0,0.0,0,3,0
EN
```

| CM GEOMETRY : QUARTER WAVELENGTH MONOPOLE |
| :---: |
| CM WITH QUARTER WAVELENGTH 4 RADIAL WIRES |
| CM ELEVATED .08LAMBDA $=8421 \mathrm{M}$ |
| CM FREQUENCY : 28.5 MHZ |
| CM WAVELENGTH (FOR SKY WAVES) $=10.5263 \mathrm{M}$ |
| CM WAVELENGTH (FOR GROUND WAVES) $=3.299 \mathrm{M}$ |
| CM WIRE : 非12 ( RADIUS R=.010265M) |
| CM GROUND (0) : EPSILON $=10 \quad$ SIGMA $=.003$ |
| CE |
| GW 1, 10, $0,0.8421,2.6316,0, .8421, .010265$ |
| GR 0,4 |
| GW 2, 10, 0,0,.8421, 0,0,3.4737, 010265 |
| GW 3,1, 0,0,.8321, 0,0,0,.010265 |
| GW 4,5, 0,0,0, 0,0, -1.2192, . 010265 |
|  |
| FR 0,0,0,0,28.5 |
| GN 2,0,0,0,10,. 003 |
| EX 0,2,1,01,1,0 |
| PL3, 2, 1,0 |
| RP1, 1, 121, 0, 7. 62, 0. 0, 0, 3, 1609.3 |
| PL3,2,2,0 |
| RP1, 1, 121, 0, 7. 62, 0.0,0,3,1609.3 |
| PLO, $0,0,0$ |
| RP0,1,121,1500, $80,0.0,0,3,0$ |
| RP0, 1, 121, 1500, $70,0.0,0,3,0$ |
| RPO $, 1,121,1500,60,0.0,0,3,0$ |
| RP0, 1, 121, 1500, 50, 0.0,0,3,0 |
| RP0,1,121,1500,40,0.0,0,3,0 |
| RP0, 1, 121, 1500, 30, $0.0,0,3,0$ |
| RP0, 1, 121, 1500, 20, $0.0,0,3,0$ |
| RP0, 1, 121, 1500, 10, $0.0,0,3,0$ |
| RP0, 1, 121,1500, $0,0.0,0,3,0$ |
| EN |

CM GEOMETRY : QUARTER WAVELENGTH MONOPOLE

| $C M$ | WITH QUARTER WAVELENGTH 15 RADIAL WIRES |
| :--- | :--- |
| $C M$ | ELEVATED .O8LAMBDA $=.8421 M$ |

```
GW 1,10, 0,0,.8421, 2.6316,0,.8421,.010265
GR 0,15
GW 2,10, 0,0,.8421, 0,0,3.4737,.010265
GW 3,1, 0,0,.8321, 0,0,0,.010265
GW 4,5, 0,0,0, 0,0,-1.2192,.010265
GE O
FR 0,0,0,0,28.5
GN 2,0,0,0,10,.003
EX 0,2,1,01,1,0
PL3,2,1,0
RP1,1,121,0,7.62,0.0,0,3,1609.3
PL3,2,2,0
RP1,1,121,0,7.62,0.0,0,3,1609.3
PLO,0,0,0
RPO,1,121,1500,80,0.0,0,3,0
RPO,1,121,1500,70,0.0,0,3,0
RPO,1,121,1500,60,0.0,0,3,0
RPO,1,121,1500,50,0.0,0,3,0
RP0,1,121,1500,40,0.0,0,3,0
RPO,1,121,1500,30,0.0,0,3,0
RPO,1,121,1500,20,0.0,0,3,0
RPO,1,121,1500,10,0.0,0,3,0
RPO,1,121,1500,0,0.0,0,3,0
EN
CM GEOMETRY : QUARTER WAVELENGTH MONOPOLE
CM WITH QUARTER WAVELENGTH 30 RADIAL WIRES
CM ELEVATED . O8LAMBDA=. 84?1M
CM FREQUENCY : 28.5NHZ
CM WAVELENGTH (FOR SKY WAVES) = 10.5263M
CM WAVELENGTH (FOR GROUND WAVES) = 3.299M
CM WIRE : #12 ( RADIUS R=.010265M )
CM GROUND(0) : EPSILON = 10 SIGMA=.003
CE
GW 1,5, 0,0,.8421, 2.6316,0,.8421, . }01026
GR 0,30
GW 2,10, 0,0,.8421, 0,0,3.4737,.010265
GW 3,1, 0,0,.8321, 0,0,0,.010265
GW 4,5, 0,0,0, 0,0,-1.2192,.010265
GE O
FR 0,0,0,0,28.5
GN 2,0,0,0,10,.003
EX 0,2,1,01,1,0
PL3,2,1,0
RP1,1,121,0,7.62,0.0,0,3,1609.3
PL3,2,2,0
RP1,1,121,0,7.62,0.0,0,3,1609.3
PLO,0,0,0
RP0,1,121,1500,80,0.0,0,3,0
RP0,1,121,1500,70,0.0,0,3,0
RP0,1,121,1500,60,0.0,0,3,0
RPO,1,121,1500,50,0.0,0,3,0
RP0,1,121,1500,40,0.0,0,3,0
RP0,1,121,1500,30,0.0,0,3,0
RP0,1,121,1500,20,0.0,0,3,0
RP0,1,121,1500,10,0.0,0,3,0
```

RPO , 1, 121, 1500, 0, 0. 0, 0, 3, 0
EN

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